CONTACT PROBLEM FOR BONDED NONHOMOGENEOUS MATERIALS UNDER SHEAR LOADING

B. M. SINGH, J. ROKNE, R. S. DHALIWAL, and J. VRBIK

The present paper examines the contact problem related to shear punch through a rigid strip bonded to a nonhomogeneous medium. The nonhomogeneous medium is bonded to another nonhomogeneous medium. The strip is perpendicular to the y-axis and parallel to the x-axis. It is assumed that there is perfect bonding at the common plane surface of two nonhomogeneous media. Using Fourier cosine transforms, the solution of the problem is reduced to dual integral equations involving trigonometric cosine functions. Later on, the solution of the dual integral equations is transformed into the solution of a system of two simultaneous Fredholm integral equations of the second kind. Solving numerically the Fredholm integral equations of the second kind, the numerical results of resultant contact shear are obtained and graphically displayed to demonstrate the effect of nonhomogeneity of the elastic material.

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1. Introduction. In practical applications, the material nonhomogeneity becomes an important factor to be considered, particularly, in the certain class of problems such as the foundation and contact problems in soil mechanics and wave propagation problems in the mechanics. In solid mechanics, many of the engineering materials, such as composites and large variety of bonded material and structural components, are generally modeled as nonhomogeneous continua. An example of a material with these properties is shale-sandstone. There are some important applications in ceramic coating of metal substrates and in metal-ceramic composites with graded properties. The advantages of functionally gradient materials are that of the materials which can resist high temperatures effectively and the thermal stresses in the material can be reduced significantly. Therefore, those materials cannot break easily and they have important applications in engineering.

Related to the present work is the solution of the mixed boundary value problems in nonhomogeneous medium discussed by Singh [4], Dhaliwal and Singh [2], and Delale and Erdogan [1]. In these papers, the nonhomogeneity vary in the two directions of the coordinate axes. It is important to mention that Erdogan [3] discussed crack problems under antiplane shear loading in bonded materials, where shear moduli vary exponentially as a function of x. Even though, no systematic study of the problem discussed in this paper

appears to have been made, it is reasonable to expect that, in nonhomogeneous materials with continuous and continuously differentiable elastic constants, the nature of stress singularity at the punch corner would be identical to that of a homogeneous medium.

In this paper, we consider the finite antiplane shear punch on the nonhomogeneous medium $0 < x < \infty$ and $0 < y < \infty$. The medium has shear modulus $\mu(x,y) = G_1 e^{\alpha_1 x + \beta y}$ and the medium is bonded by another nonhomogeneous medium $-\infty < x < 0$ with shear modulus $\mu(x) = G_2 e^{\alpha_2 x}$. The formulation of the problem leads to the solution of dual integral equations with trigonometric cosine function. Finally, the solution of the problem is reduced to the solution of two simultaneous system of Fredholm integral equations of the second kind in two unknown functions. The expressions for shear stress and resultant shear force under the punch are obtained. The simultaneous system of Fredholm integral equations is numerically solved and numerical values for resultant shear force under the punch and shear stress are graphed to demonstrate the effect of nonhomogeneity of the elastic material.

This paper also contains a novel treatment of contact problems involving a nonhomogeneous space and has practical value in soil mechanics and mining engineering. This paper has importance for the study of some materials that are nonhomogeneous in the x and y directions.

2. Solution of equilibrium equation in rectangular Cartesian coordinates.
We consider a solid under shear such that the displacement field is given by

$$u_x(x,y,z) = 0, \qquad u_y(x,y,z) = 0, \qquad u_z(x,y,z) = w(x). \qquad (2.1)$$

The only nonzero stress components are given by

$$\sigma_{xz}(x,y) = \mu \frac{\partial w}{\partial x}, \qquad \sigma_{yz}(x,y) = \mu \frac{\partial w}{\partial y}, \qquad (2.2)$$

where μ, the modulus of rigidity of the material, is assumed to be continuous and twice differentiable function of x and y. In this case, the equation of equilibrium of an isotropic elastic material in the absence of body force is given by

$$\frac{\partial}{\partial x}\left(\mu \frac{\partial w}{\partial x}\right) + \frac{\partial}{\partial y}\left(\mu \frac{\partial w}{\partial y}\right) = 0. \qquad (2.3)$$

If we take

$$w(x,y,z) = \frac{W(x,y)}{\sqrt{\mu(x,y)}}, \qquad (2.4)$$

then making use of (2.4), (2.3) takes the following form:

$$\mu\Delta^2 W + \frac{1}{2}\left[\frac{1}{2\mu}\left\{\left(\frac{\partial\mu}{\partial x}\right)^2 + \left(\frac{\partial\mu}{\partial y}\right)^2\right\} - \frac{\partial^2\mu}{\partial x^2} - \frac{\partial^2\mu}{\partial y^2}\right]W = 0, \qquad (2.5)$$

where, in Cartesian coordinates, the Laplacian operator Δ^2 takes the form

$$\Delta^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}. \qquad (2.6)$$

Now assume that W and μ can be taken in the form

$$W(x,y) = X(x)Y(y), \qquad \mu = \mu_0 p(x)q(y), \qquad (2.7)$$

where μ_0 is a constant. Substituting (2.7) into (2.5) for W and μ, we find that X and Y satisfy the following differential equations:

$$X_{xx} + \left[k^2 + \frac{1}{4}\left(\frac{p_x}{p}\right)^2 - \left(\frac{p_{xx}}{p}\right)\right]X = 0,$$
$$Y_{yy} + \left[-k^2 + \frac{1}{4}\left(\frac{q_y}{q}\right)^2 - \left(\frac{q_{yy}}{q}\right)\right]Y = 0, \qquad (2.8)$$

where

$$p_x = \frac{\partial p}{\partial x}, \qquad p_{xx} = \frac{\partial^2 p}{\partial x^2}, \qquad (2.9)$$

and k is a separating constant. If we assume that

$$\frac{p_{xx}}{2p} - \frac{1}{4}\left(\frac{1}{p}\frac{dp}{dx}\right)^2 = a_0, \qquad \frac{q_{yy}}{2p} - \frac{1}{4}\left(\frac{1}{q}\frac{dq}{dy}\right)^2 = b_0, \qquad (2.10)$$

where a_0 and b_0 are constants, we find that (2.8) can be written in the form

$$X_{xx} + (k^2 - a_0)X = 0,$$
$$Y_{yy} - (k^2 + b_0)Y = 0. \qquad (2.11)$$

Making use of (2.4), (2.7), and (2.11), we find the displacement component. To find the solution of (2.11), we take the variable separation constant in the following form:

$$\xi^2 = k^2 - a_0, \qquad (2.12)$$

and write (2.11) in the following form:

$$X_{xx} + \xi^2 X = 0,$$
$$Y_{yy} - [\xi^2 + a_0 + b_0]Y = 0. \tag{2.13}$$

The solution of (2.13) can be written as

$$A(\xi)\cos(\xi x)e^{-(\xi^2+a_0+b_0)^{1/2}y}, \tag{2.14}$$

where $A(\xi)$ is an arbitrary constant.

An alternative solution of (2.11) can be written if we write the variable separable constant in the form

$$\xi^2 = k^2 + b_0, \tag{2.15}$$

then the solution of (2.11) can be taken as

$$B(\xi)\cos(\xi y)e^{-(\xi^2+a_0+b_0)^{1/2}x}, \tag{2.16}$$

where $B(\xi)$ is an arbitrary constant. In particular, we take the shear modulus in the form

$$\mu_1 = G_1 e^{\alpha_1 x + \beta y} \tag{2.17}$$

for the region 1 ($0 < x < \infty$, $0 < y < \infty$), then comparing (2.17) with (2.7), we find that

$$\mu_0 = G_1, \qquad p(x) = e^{\alpha_1 x}, \qquad q(y) = e^{\beta y}. \tag{2.18}$$

We can easily find from (2.10) that

$$a_0 = \frac{\alpha_1^2}{4}, \qquad b_0 = \frac{\beta^2}{4}. \tag{2.19}$$

Making use of (2.4), (2.14), (2.16) and (2.19), we find the expression for displacement component for the region ($0 < x < \infty$, $0 < y < \infty$) in the following form:

$$w^1(x,y) = \frac{1}{\sqrt{G_1 e^{\alpha_1 x + \beta y}}} \left[\int_0^\infty \left\{ A(\xi)\cos(\xi x)e^{-(\xi^2+(\alpha_1^2+\beta^2)/4)^{1/2}y} \right.\right.$$
$$\left.- B(\xi)\left(\frac{\sin(\xi y)}{\xi} + \frac{2}{\beta}\cos(\xi y)\right) \tag{2.20}\right.$$
$$\left.\left.\times e^{-(\xi^2+(\alpha_1^2+\beta^2)/4)^{1/2}x} \right\} d\xi \right],$$

where $A(\xi)$ and $B(\xi)$ are arbitrary functions of ξ. The corresponding shear stress components for the region $(0 < x < \infty, \; 0 < y < \infty)$ are as follows:

$$\sigma_{yz}^1(x,y) = -\sqrt{G_1 e^{\alpha_1 x + \beta y}} \left[\int_0^\infty A(\xi) \left\{ \left(\xi^2 + \frac{\alpha_1^2 + \beta^2}{4} \right)^{1/2} + \frac{\beta}{2} \right\} \right.$$
$$\times \cos(\xi x) e^{-(\xi^2 + (\alpha_1^2 + \beta^2)/4)^{1/2} y} \tag{2.21}$$
$$\left. - B(\xi) \frac{4\xi^2 + \beta^2}{2\xi\beta} \sin(\xi y) e^{-(\xi^2 + (\alpha_1^2 + \beta^2)/4)^{1/2} x} \right] d\xi$$

$$\sigma_{xz}^1(x,y) = -\sqrt{G_1 e^{\alpha_1 x + \beta y}} \left[\int_0^\infty \left\{ A(\xi) \left(\frac{\alpha_1}{2} \cos(\xi x) + \frac{\xi}{2} \sin(\xi x) \right) \right. \right.$$
$$\times e^{-(\xi^2 + (\alpha_1^2 + \beta^2)/4)^{1/2} y}$$
$$- \left(\left(\xi^2 + \frac{\alpha_1^2 + \beta^2}{4} \right)^{1/2} + \frac{\alpha_1}{2} \right) \tag{2.22}$$
$$\times B(\xi) e^{-(\xi^2 + (\alpha_1^2 + \beta^2)/4)^{1/2} x}$$
$$\left. \left. \times \left(\frac{\sin(\xi y)}{\xi} + \frac{2}{\beta} \cos(\xi y) \right) \right\} d\xi \right].$$

For region 2, we assume that the shear modulus is as follows:

$$\mu_2 = G_2 e^{\alpha_2 x} \quad (-\infty < x < 0). \tag{2.23}$$

For the solution of equilibrium equation (2.5) for the region 2, we can easily write the displacement and shear stress components, for the region $-\infty < x < 0$, $0 < y < \infty$, in the following integral form:

$$w^2(x,y) = \frac{1}{\sqrt{G_2 e^{\alpha_2 x}}} \left[\int_0^\infty C(\xi) e^{(\xi^2 + (\alpha_2^2/4))^{1/2} x} \cos(\xi y) d\xi \right], \tag{2.24}$$

$$\sigma_{yz}^2(x,y) = -\sqrt{G_2 e^{\alpha_2 x}} \left[\int_0^\infty \xi C(\xi) e^{(\xi^2 + (\alpha_2^2 + \beta^2)/4)^{1/2} x} \sin(\xi y) d\xi \right], \tag{2.25}$$

$$\sigma_{xz}^2(x,y) = \sqrt{G_2 e^{\alpha_2 x}} \left[\int_0^\infty \left[\left(\xi^2 + \frac{\alpha_2^2 + \beta^2}{4} \right)^{1/2} - \frac{\alpha_2}{2} \right], \right.$$
$$\left. \times C(\xi) e^{(\xi^2 + (\alpha_2^2/4))^{1/2} x} \cos(\xi y) d\xi \right], \tag{2.26}$$

where $C(\xi)$ are arbitrary functions of ξ.

3. Statement of problem and derivation of Fredholm integral equation of the second kind.
We consider the problem of the antiplane shear of a nonhomogeneous half-space $(0 < x < \infty, \; 0 < y < \infty)$ of a shear modulus $G_1 e^{\alpha_1 x + \beta y}$ bonded with a semi-infinite medium $-\infty < x < 0, \; y > \infty$ of shear modulus $G_2 e^{\alpha_2 x}$, where G_1, G_2, α_1, α_2, and β are real constants and x and y refer to Cartesian coordinates. Contact shear force is applied to the flat part
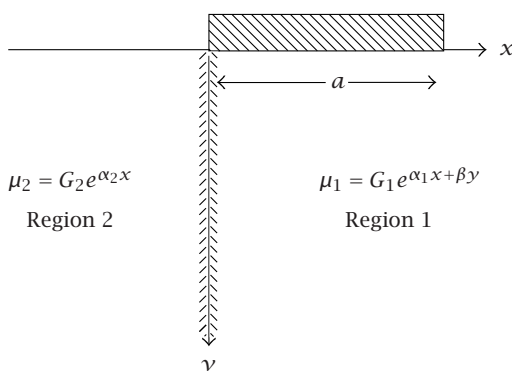
FIGURE 3.1. Contact problem for bonded nonhomogeneous materials.

of the surface $y = 0$, $0 < x < a$, through a rigid strip bounded to a nonhomogeneous medium. The geometry of the problem is shown in Figure 3.1. The boundary conditions of the problem may be taken as

$$w^1(x,0) = f(x), \quad 0 < x < a,$$
$$\sigma_{yz}^1(x,0) = 0, \quad a < x < \infty, \tag{3.1}$$

$$\sigma_{yz}^2(x,0) = 0, \quad -\infty < x < 0. \tag{3.2}$$

We have the following continuity conditions along the plane surface $x = 0$:

$$w^1(0,y) = w^2(0,y), \quad \sigma_{xz}^1(0,y) = \sigma_{xz}^2(0,y), \quad 0 < y < \infty. \tag{3.3}$$

It is required that $w^1(x,y)$ and $w^2(x,y)$ tend to zero as $\sqrt{x^2 + y^2} \to \infty$ and $f(-x) = f(x)$; $f(x)$ is a known function of x.

We find that the boundary condition (3.2) is satisfied automatically at $y = 0$. Making use of (2.20), (2.22), (2.24), and (2.26), we find, from the boundary conditions (3.3), that

$$\int_0^\infty \left[C(\xi) + \frac{2\sqrt{G}}{\beta} B(\xi) \right] \cos(\xi y)\,d\xi + \sqrt{G} \int_0^\infty \frac{B(\xi)\sin(\xi y)\,d\xi}{\xi}$$
$$= \sqrt{G} \int_0^\infty \frac{A_1(\xi)e^{-ye_1(\xi)}\,d\xi}{e_1(\xi)}, \quad 0 < y < \infty,$$

$$\sqrt{G} \int_0^\infty e_3(\xi)C(\xi)\cos(\xi y)\,d\xi - \frac{2}{\beta} \int_0^\infty e_4(\xi)B(\xi)\cos(\xi y)\,d\xi \tag{3.4}$$
$$- \int_0^\infty \frac{e_4(\xi)B(\xi)\sin(\xi y)\,d\xi}{\xi}$$
$$= -\frac{\alpha_1}{2} \int_0^\infty \frac{e^{-ye_2(\xi)}A_1(\xi)\,d\xi}{e_1(\xi)}, \quad 0 < y < \infty,$$

where

$$e_1 = \left[\left(\xi^2 + \frac{\alpha_1^2 + \beta^2}{4} \right)^{1/2} + \frac{\beta}{2} \right],$$

$$e_2 = \left[\left(\xi^2 + \frac{\alpha_1^2 + \beta^2}{4} \right)^{1/2} - \frac{\beta}{2} \right],$$

$$e_3 = \left[\left(\xi^2 + \frac{\alpha_2^2}{4} \right)^{1/2} - \frac{\alpha_2}{2} \right], \tag{3.5}$$

$$e_4 = \left[\left(\xi^2 + \frac{\alpha_1^2 + \beta^2}{4} \right)^{1/2} + \frac{\alpha_1}{2} \right],$$

$$G = \frac{G_2}{G_1}, \qquad A_1(\xi) = e_1 A(\xi). \tag{3.6}$$

Making use of Fourier cosine transforms to (3.4), we find that

$$C(\xi) + \frac{2\sqrt{G}}{\beta} B(\xi) + \frac{2\sqrt{G}}{\pi} \int_0^\infty \frac{B(u)du}{u^2 - \xi^2}$$
$$= \frac{2}{\pi} \sqrt{G} \int_0^\infty \frac{A_1(u)du}{[\xi^2 + e_1^2(u)]}, \quad 0 < \xi < \infty,$$
$$\sqrt{G} C(\xi) e_3(\xi) - \frac{2}{\beta} e_4(\xi) B(\xi) - \frac{2}{\pi} \int_0^\infty \frac{e_4(u) B(u) du}{u^2 - \xi^2} \tag{3.7}$$
$$= -\frac{\alpha_1}{\pi} \int_0^\infty \frac{e_2(u) A_1(u) du}{e_1(u)[\xi^2 + e_1^2(u)]}, \quad 0 < \xi < \infty.$$

Equations (3.7) have been obtained by using the following integrals:

$$\int_0^\infty \sin(uy) \cos(\xi y) dy = \left(\frac{u}{u^2 - \xi^2} \right),$$
$$\int_0^\infty e^{-e_1(u)y} \cos(\xi y) dy = \left(\frac{e_1(u)}{\xi^2 + e_1^2(u)} \right). \tag{3.8}$$

Eliminating $C(\xi)$ from (3.7), we get that

$$B(\xi) e_5(\xi) + \int_0^\infty \frac{B(u) K_1(u,\xi) du}{u^2 - \xi^2} = \int_0^\infty A_1(u) R_1(u,\xi) du, \quad 0 < \xi < \infty, \tag{3.9}$$

where

$$e_5(\xi) = \frac{2}{\beta} [e_4(\xi) + G c_3(\xi)],$$

$$R_1(u,\xi) = \frac{1}{\pi} \left[\frac{2G e_3(\xi)}{[\xi^2 + e_1^2(u)]} + \frac{\alpha_1 e_2(u)}{e_1(u)[\xi^2 + e_2^2(u)]} \right], \tag{3.10}$$

$$K_1(u,\xi) = \frac{2}{\pi} [e_4(u) + G e_3(\xi)].$$

Making use of (2.20) and (2.21) in the boundary conditions (3.1), we find that

$$\int_0^\infty \frac{A_1(\xi)\cos(\xi x)d\xi}{\xi} + \int_0^\infty M_1(\xi)A_1(\xi)\cos(\xi x)d\xi$$

$$- \frac{2}{\beta}\int_0^\infty B(\xi)e^{xe_6(\xi)}d\xi = \sqrt{G_1}e^{\alpha_1 x/2}f(x), \quad 0 < x < a, \quad (3.11)$$

$$\int_0^\infty A_1(\xi)\cos(\xi x)d\xi = 0, \quad a < x,$$

where

$$M_1(\xi) = \left[\frac{1}{e_1(\xi)} - \frac{1}{\xi}\right],$$

$$e_6(\xi) = -\left[\xi^2 + \frac{\alpha_1^2 + \beta^2}{4}\right]^{1/2}, \quad (3.12)$$

and $A_1(\xi)$ is defined by (3.6).

The solution of the dual integral equations (3.11) can be written as

$$A_1(\xi) = \xi(G)^{1/2}\int_0^a t\phi(t)J_1(\xi t)dt, \quad (3.13)$$

where $\phi(t)$ satisfies the following Fredholm integral equation of the second kind:

$$\phi(t) + \int_0^a \phi(u)K_2(u,t)du$$

$$+ \frac{2}{\beta}\int_0^\infty e_6(\xi)\left[\frac{2}{\pi} + I_1(e_6 t) + L_1(e_6 t)\right]B_1(\xi)d\xi \quad (3.14)$$

$$= \frac{-\alpha_1}{2}\left[I_1\left(\frac{\alpha_1 t}{2}\right) + L_1\left(\frac{\alpha_1 t}{2}\right) + \frac{2}{\pi}\right], \quad 0 < t < a,$$

and

$$K_2(u,t) = u\int_0^\infty \xi^2 M_1(\xi)J_1(\xi u)J_1(\xi t)d\xi, \quad (3.15)$$

$$\sqrt{G_1}B_1(\xi) = B(\xi). \quad (3.16)$$

For obtaining (3.14), we have taken $f(x) = 1$ and we have used the following results:

$$\frac{d}{dt}\int_0^t \frac{\cos(\xi x)dx}{(t^2 - x^2)^{1/2}} = -\left(\frac{\pi\xi}{2}\right)J_1(\xi t),$$

$$\frac{d}{dt}[L_0(e_6 t)] = e_6\left[\frac{2}{\pi} + L_1(te_6)\right], \quad (3.17)$$

$$\frac{d}{dt}\int_0^t \frac{e^{xe_6}dx}{(t^2 - x^2)^{1/2}} = \frac{\pi e_6}{2}\left[\frac{2}{\pi} + I_1(e_6 t) + L_1(e_6 t)\right],$$
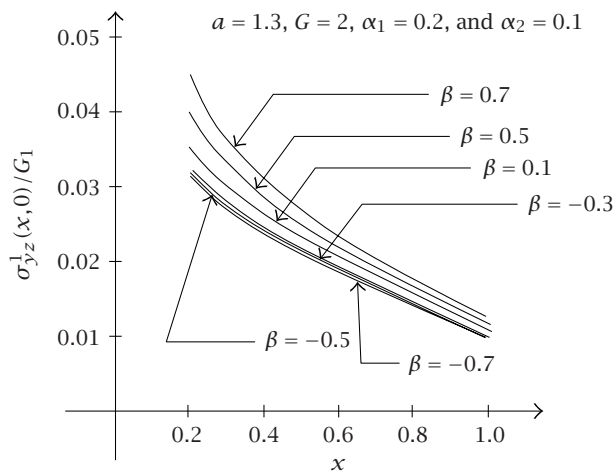
FIGURE 3.2. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\beta = -0.7, -0.5, -0.3, 0.1, 0.5, 0.7$, $a = 1.3$, $G = 2$, $\alpha_1 = 0.2$, and $\alpha_2 = 0.1$.
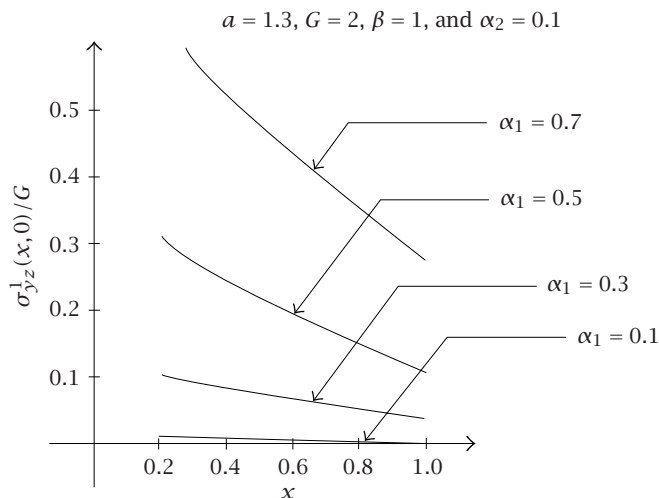

FIGURE 3.3. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\alpha_1 = 0.1, 0.3, 0.5, 0.7$, $a = 1.3$, $G = 2$, $\alpha_2 = 0.1$, and $\beta = 1$.

where $J_1()$ and $I_1()$ are, respectively, the Bessel functions of the first kind and modified Bessel functions of the first kind, and $L_1()$ denotes the Struve function of the first kind of order one.

Making use of (3.13) and (3.16), (3.9) can be written in the following form:

$$B_1(\xi)e_5(\xi) + \int_0^\infty \frac{B_1(u)K_1(u,\xi)du}{u^2 - \xi^2} = \int_0^a \phi(t)N_1(t,\xi)dt, \quad 0 < \xi < \infty, \quad (3.18)$$
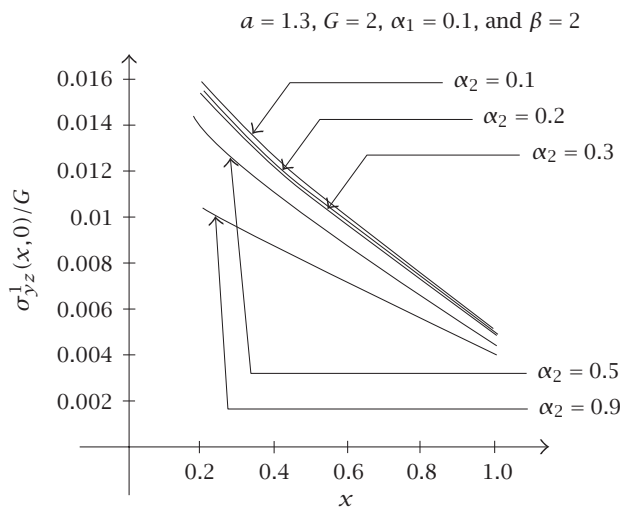
$a = 1.3$, $G = 2$, $\alpha_1 = 0.1$, and $\beta = 2$

FIGURE 3.4. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\alpha_2 = 0.1, 0.3, 0.5, 0.7, 0.9$, $a = 1.3$, $G = 2$, $\alpha_1 = 0.1$, and $\beta = 2$.
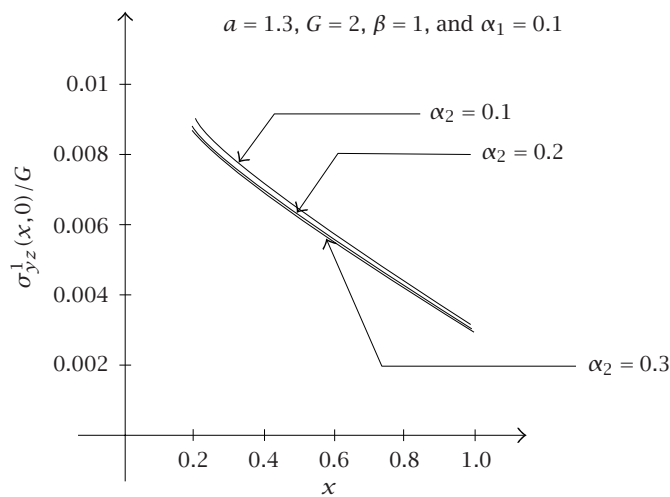
$a = 1.3$, $G = 2$, $\beta = 1$, and $\alpha_1 = 0.1$

FIGURE 3.5. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\alpha_2 = 3, 5, 7, 9$, $a = 1.3$, $G = 2$, $\alpha_1 = 0.1$, and $\beta = 2$.

where

$$N_1(t,\xi) = t \int_0^\infty u J_1(u,t) R_1(u,\xi) du. \tag{3.19}$$

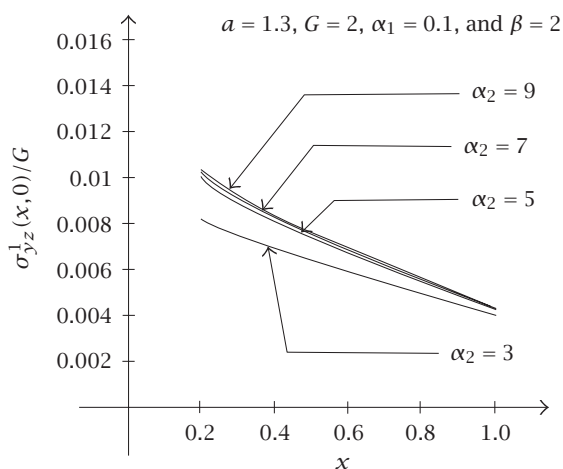Equations (3.14) and (3.18) are simultaneous Fredholm equations of the second kind.

FIGURE 3.6. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\alpha_2 = 3,5,7,9$, $a = 1.3$, $G = 2$, $\alpha_1 = 0.1$, and $\beta = 2$.
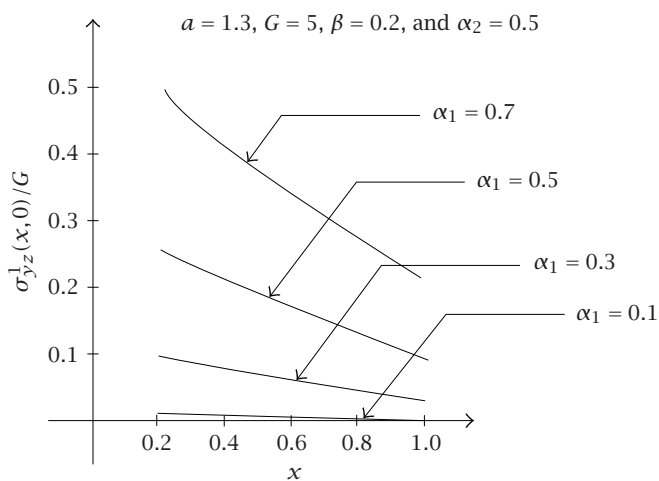

FIGURE 3.7. Variation of $\sigma_{yz}^1(x,0)/G_1$ with x for different values of $\alpha_1 = 0.1,0.3,0.5,0.7$, $a = 1.3$, $G = 5$, $\alpha_2 = 0.5$, and $\beta = 0.2$.

Making use of (2.21) and (3.6), we find that

$$
\begin{aligned}
\sigma_{yz}^1(x,0) &= -\sqrt{G_1}\, e^{\alpha_1 x/2} \int_0^\infty A_1(\xi)\cos(\xi x)\, d\xi \\
&= -\sqrt{G_1}\, e^{\alpha_1 x/2} \frac{d}{dx} \int_0^\infty \frac{A_1(\xi)\sin(\xi x)\, d\xi}{\xi}, \quad 0 < x < a.
\end{aligned}
\tag{3.20}
$$

Substituting the value of $A_1(\xi)$ from (3.13) into (3.20), we find that

$$\frac{\sigma_{yz}^1(x,0)}{G_1} = -e^{\alpha_1 x/2}\frac{d}{dx}\left[x\int_x^a\frac{\phi(t)dt}{(t^2-x^2)^{1/2}}\right], \quad 0 < x < a. \tag{3.21}$$

Solving numerically the simultaneous Fredholm integral equations (3.14) and (3.18) to get the values of $\phi(t)$ and finally using expression (3.21), we get the numerically results for $\sigma_{yz}^1(x,0)/G_1$ which are plotted in Figures 3.2, 3.3, 3.4, 3.5, 3.6, and 3.7.

We notice from Figure 3.2 that the shear stress on the surface of the elastic material under the rigid strip decreases with x. Also we notice the following trend for the shear stress with the nonhomogeneity constants β, α_1, and α_2: $\sigma_{yz}^1(x,0)/G_1$ increases with β in Figure 3.2, increases with α_1 in Figures 3.3, 3.7, decreases with $\alpha_2 < 1$ in Figures 3.4, 3.5, and increases with $\alpha_2 > 1$ in Figure 3.6.

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Special Issue on
Decision Support for Intermodal Transport

Call for Papers

Intermodal transport refers to the movement of goods in a single loading unit which uses successive various modes of transport (road, rail, water) without handling the goods during mode transfers. Intermodal transport has become an important policy issue, mainly because it is considered to be one of the means to lower the congestion caused by single-mode road transport and to be more environmentally friendly than the single-mode road transport. Both considerations have been followed by an increase in attention toward intermodal freight transportation research.

Various intermodal freight transport decision problems are in demand of mathematical models of supporting them. As the intermodal transport system is more complex than a single-mode system, this fact offers interesting and challenging opportunities to modelers in applied mathematics. This special issue aims to fill in some gaps in the research agenda of decision-making in intermodal transport.

The mathematical models may be of the optimization type or of the evaluation type to gain an insight in intermodal operations. The mathematical models aim to support decisions on the strategic, tactical, and operational levels. The decision-makers belong to the various players in the intermodal transport world, namely, drayage operators, terminal operators, network operators, or intermodal operators.

Topics of relevance to this type of decision-making both in time horizon as in terms of operators are:

- Intermodal terminal design
- Infrastructure network configuration
- Location of terminals
- Cooperation between drayage companies
- Allocation of shippers/receivers to a terminal
- Pricing strategies
- Capacity levels of equipment and labour
- Operational routines and lay-out structure
- Redistribution of load units, railcars, barges, and so forth
- Scheduling of trips or jobs
- Allocation of capacity to jobs
- Loading orders
- Selection of routing and service

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